

Photonic Integrated Circuits: a Study on Process Variations

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Abstract: Developing an efficient method and applying it to study several identical microresonators fabricated by electron beam lithography, we quantify the worst-case within-die silicon thickness and resonance wavelength variations to be 1.55 and 2.11 nm, respectively.

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1. Introduction

Designing silicon photonic integrated circuits (PICs) for wavelength-division multiplexing (WDM)-based applications requires a careful consideration of process variations. The functionality of such systems is highly tied to how well different devices are matched in terms of their central wavelengths. Some efforts have been made to characterize process variations in PICs [1–4], in which within-die, within-wafer, and wafer-to-wafer variations have been explored. Also, the silicon thickness variation is identified as the major concern. This paper presents a systematic perspective through developing a computationally efficient method to study the impact of process variations on large-scale PICs. Compared with time-consuming numerical simulations, we demonstrate that our proposed method is highly efficient in terms of accuracy and computation time: an error rate of smaller than 1% and a speed-up of greater than $100\times$ are achieved. Employing the proposed method, we study 60 identical microresonators (MRs) on a 2.1×4.5 mm² chip fabricated by the electron beam lithography system at the university of Washington with a high resolution of 2 nm. Our study quantifies the worst-case within-die silicon thickness variation and resonance wavelength shift to be 1.55 and 2.11 nm, respectively. Moreover, not only do we confirm a strong correlation among the resonance wavelengths of the MRs in proximity as in [1], but also we demonstrate that the same correlation can exist among the MRs which are not in proximity. The proposed method helps evaluate the impact of process variations on the performance of large-scale PICs, determining power penalties required to trim/tune (e.g., thermal tuning) faulty devices in such systems.

2. Theory

It is possible to consider design parameters sweeps (a.k.a. corner analysis) in a numerical simulation (e.g., FDTD simulation) of a photonic device. However, employing such simulations for large-scale PICs is not feasible due to the computation cost. Our novel contribution is to develop a fast and accurate method to study large-scale PICs under random process variations. Considering an extended version of Marcatili's approach [5], we develop an analytical

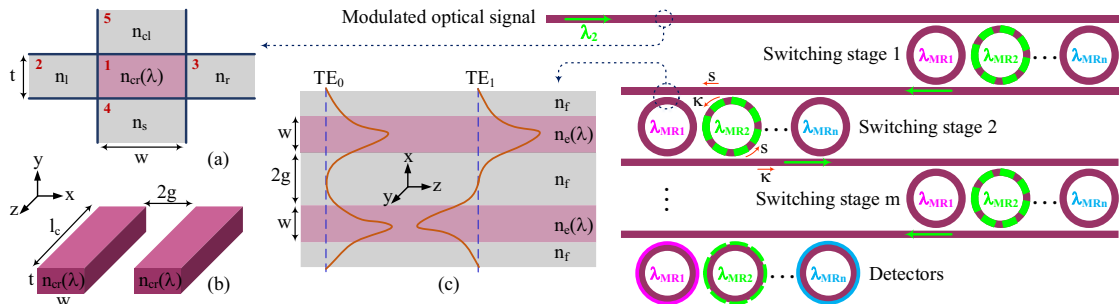


Fig. 1: An illustration of various aspects of a large-scale PIC for WDM-based applications with n wavelengths and m switching stages. All the functional devices utilize MRs, including wavelength-selective photodetectors and photonic switches. (a) 2D approximation of a strip waveguide based on Marcatili's approach; (b) Coupling region in photonic switches; and, (c) 2D approximation of the coupler including the symmetric and antisymmetric supermodes.

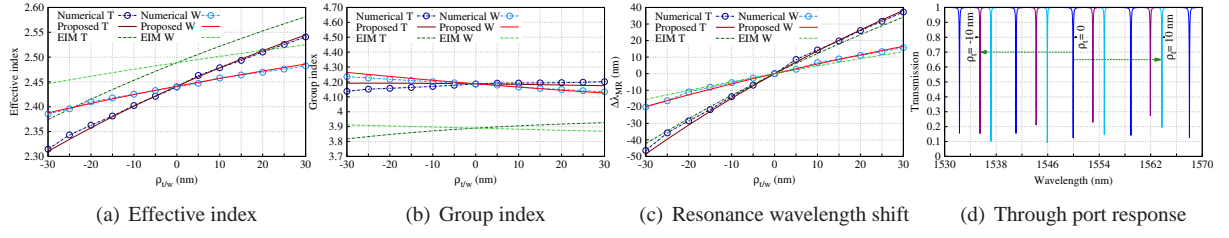


Fig. 2: Quantitative simulation results of the proposed models, and comparisons with the results from numerical simulations, performed in Lumerical MODE, and the effective index method (EIM). "T" and "W" stand for thickness and width variations, respectively. The resonance wavelength shift in (c) is independent of the MR radius. (d) Optical spectrum of our fabricated TE polarization MR calculated using the proposed method with $r = 10 \mu\text{m}$, $l_c \simeq 1 \mu\text{m}$, $2g = 200 \text{ nm}$, and $\lambda_{MR}^0 = 1550 \text{ nm}$ under $\rho_t = \pm 10 \text{ nm}$.

method to study the effective and group indices of the fundamental TE mode in strip waveguides under silicon thickness and waveguide width variations. Applying the developed method, Fig. 1(a) illustrates a 2D approximation of a strip waveguide with a thickness and width of t and w , respectively. The waveguide core, region 1, is silicon with a refractive index of $n_{cr}(\lambda)$, where Sellmeier equation is considered to take into account the the impact of material dispersion. The surrounding regions are all from SiO_2 with $n_l = n_r = n_s = n_{cl} = 1.444$, in which the dispersion is ignored as the light is mostly confined in the waveguide core.

Finding a solution to E_z and H_z in region 1 that assumes the electric fields (E_x) to be predominantly polarized in the y-direction to satisfy Maxwell's equations, we can calculate the effective index of the waveguide as $n_{eff}(T, W, \lambda) = \frac{\lambda}{2\pi} \sqrt{n_{cr}^2(\lambda)k_0^2 - k_x^2(T, W, \lambda) - k_y^2(T, W, \lambda)}$. Here, T and W are the thickness and width of the waveguide under variations and they are equal to $t \pm \rho_t$ and $w \pm \rho_w$, respectively. We define ρ_t and ρ_w to take into account the variations in the silicon thickness and waveguide width, respectively. It is worth mentioning that $\rho_{t/w}$ can be assigned by a random number generator function that respects the mean and standard deviation of the variations measured in different fabrications. k_x and k_y are the spatial frequencies that can be found by solving eigenvalue equations for the TM and TE modes in slab waveguides, and k_0 is the free-space wavenumber. Considering the waveguide and material dispersion, the group index can be defined as $n_g(T, W, \lambda) = n_{eff}(T, W, \lambda) - \lambda \frac{dn_{eff}(T, W, \lambda)}{d\lambda}$.

In this specific study using this method, we look at the resonance wavelength shift in MR-based photonic switches under process variations (see Fig. 1). The MR is on resonance when the round-trip optical phase, ϕ_{rt} , is an integer multiple of 2π , i.e., $\phi_{rt}(T, W, \lambda_{MR}) = \frac{2\pi n_{eff}(T, W, \lambda_{MR}) L_{rt}}{\lambda_{MR}} = m2\pi$, where L_{rt} is the optical round-trip length that equals $2\pi r(T, W) + 2l_c$. Here, $r(T, W)$ is the MR radius under silicon thickness and width variations and l_c is the coupler length (see Fig. 1(b)). Considering the first-order approximation of the waveguide dispersion (since $\frac{\partial n_{eff}}{\partial \lambda} \neq 0$), we can calculate the resonance wavelength shift as $\Delta\lambda_{MR} = \frac{\Delta\rho_{t/w} n_{eff} \lambda_{MR}^0}{n_g(t, w, \lambda_{MR}^0)}$, where λ_{MR}^0 is the initial resonance wavelength with no variations, and $\Delta\rho_{t/w} n_{eff}$ is the effective index variations under the thickness and waveguide width variations.

As Fig. 1(b) indicates, the coupling region in MR-based photonic switches consists of two directional couplers (DCs). We consider supermode theory to study the straight-through coefficient, s , and the cross-over coupling coefficient, κ , in a DC (see Fig. 1). We assume a symmetric and lossless coupler, i.e., $\kappa^2 + s^2 = 1$, while the optical losses of the coupler are incorporated into the round trip loss of the entire optical cavity. The effective indices of the first two eigenmodes of the coupled waveguides (TE_0 , symmetric, and TE_1 , antisymmetric, modes in Fig. 1(c)) determine the coefficients: $\kappa(T, W, \lambda) = \left| \sin \left(\frac{[n_{effTE_0}(T, W, \lambda) - n_{effTE_1}(T, W, \lambda)] \pi l_c}{\lambda} \right) \right|$. Here, $n_{effTE_{0/1}}$ can be calculated based on the 2D approximation of the DC indicated in Fig. 1(c) (i.e., a five-layer slab waveguide structure), in which $n_e(\lambda)$ is the effective index of the slab waveguide in the y direction in Fig. 1(b), and $n_f = 1.444$. The optical spectra of the photonic switches under variations can be simply calculated using the methodology presented in this section.

3. Results, Fabrication and Discussion

The quantitative simulation results of the proposed models, performed in MATLAB, are indicated in Fig. 2. We consider strip waveguides with $w = 500$ and $t = 220 \text{ nm}$ (same in our fabrication), and a variation range of $\rho_{t/w} \in [-30, 30] \text{ nm}$ (only in our simulations). Also, the central wavelength, λ , is at 1550 nm . As the figure indicates, compared with the numerical simulation results, our method indicates very high accuracy with an error rate of smaller than 1%. Particularly, our method achieves a speed-up of greater than $100\times$. Fig. 3(a) illustrates the unit cell of the fabricated

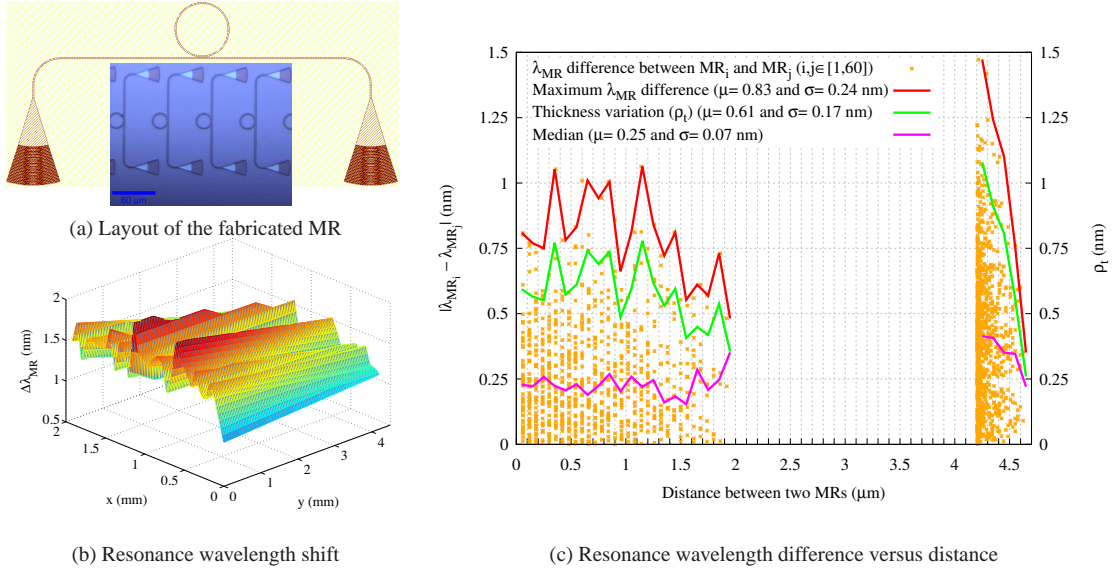


Fig. 3: (a) The unit cell of the fabricated MR (top) with a microscopic photo from part of the chip; (b) Resonance wavelength shift for devices placed at different positions (x and y) on the chip when $\lambda_{MR}^0 = 1550$ nm; and, (c) Difference in the resonance wavelengths of each MR pair (MR_i and MR_j) with respect to their distance, where 1770 comparisons are made (orange data points). The purple line indicates the median, while the green line indicates the thickness variation (ρ_t) associated with the maximum resonance wavelength difference depicted by the red line.

MR with two fiber grating couplers (FGCs) designed for 1550 nm quasi-TE operation on a 127 μm pitch. 60 copies of the same MR are placed between 60 μm and 4.2 mm apart on the chip. The optical spectrum of the fabricated MR is depicted in Fig. 2(d) (when $\rho_t = 0$), in which $\lambda_{MR}^0 = 1550$ nm and the free-spectral-range (FSR) $\simeq 9$ nm. All of the devices are automatically tested and compared with each other to study the difference in their resonance wavelengths with respect to their distance on the chip; (60 choose 2) = 1770 comparisons are made.

The resonance wavelength shift was found to be smaller than the FSR of the MR. Fig. 3(b) indicates the resonance wavelength shift (i.e., $\Delta\lambda_{MRi} = \lambda_{MRi} - \lambda_{MR}^0$ nm for $i \in [1, 60]$) versus the physical position of the MRs (see also Fig. 2(c)). We can attribute the deviations to the thickness variation as $\rho_t \gg \rho_w$ [1–3]. Since $\Delta\lambda_{MR} > 0$, based on our study $\rho_t > 0$ (i.e., thickness is 220 + ρ_t nm). The worst- and best-case $\Delta\lambda_{MR}$ (ρ_t) are found to be 2.11 (1.55) and 0.64 (0.47) nm, respectively. We indicate the resonance wavelength difference (with its maximum and median) for each pair of MRs (y axis) versus their physical distance (x axis) in Fig. 3(c). Considering the median and its standard deviation ($\sigma = 0.07$ nm), we can observe a strong correlation between the resonance wavelengths of the MRs and their distance, both for the MRs in proximity (< 2 mm) and for those > 4 mm apart. Fig. 3(c) also indicates a variability of 0.24 nm for two MRs at a distance 0 apart. Employing our method, the thickness variation (with μ [mean] = 0.61 and $\sigma = 0.17$ nm) associated with the maximum resonance wavelength difference is depicted in Fig. 3(c). The thickness varies with a small deviation in Fig. 3(c) which results in the strong correlation among the resonance wavelengths of the MRs.

The proposed method in this work can be integrated into different silicon photonics design tools, enabling the real-time performance evaluation of PICs under process variations. As a case study, we applied our method to an MR-based photonic switch consisting of four MRs for switching four wavelengths, and we found out that the optical signal-to-noise ratio (OSNR) at the drop port of the switch decreases by 7 dB on average when $\rho_t = 1.55$ nm.

References

1. L. Chrostowski *et al.*, “Impact of fabrication non-uniformity on chip-scale silicon photonic integrated circuits,” in “Optical Fiber Communication Conference,” (Optical Society of America, 2014), p. Th2A.37.
2. R. G. Beausoleil *et al.*, “Devices and architectures for large-scale integrated silicon photonics circuits,” *Proceeding of SPIE* **7942**, 1–6 (2011).
3. W. A. Zortman *et al.*, “Silicon photonics manufacturing,” *Optical Express* **18**, 598–607 (2010).
4. X. Chen *et al.*, “Process variation in silicon photonic devices,” *Applied Optics* **52**, 7638–7647 (2013).
5. W. J. Westerveld *et al.*, “Extension of marcatili’s analytical approach for rectangular silicon optical waveguides,” *Journal of Lightwave Technology* **30**, 2388–2401 (2012).